PROVINCE OF MANITOBA

DEPARTMENT OF MINES



AND NATURAL RESOURCES

WATER CONTROL AND CONSERVATION BRANCH

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HYDROMETEOROLOGICAL NETWORKS

AND

FLOOD FORECASTING PROCEDURES

FOR

OPERATION OF THE RED RIVER FLOODWAY

Winnipeg, Manitoba

October, 1971.

Prepared by:

Planning Division.

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INTRODUCTION

The Red River has a history of periodic flooding which has caused, from time to time, large property damage and human misery to the people of Manitoba. After the major flood during the spring of 1950, a concerted effort was made to develop methods whereby some advance warning could be given of potentially dangerous flood situations. A full-scale study of the Red River was undertaken by the Canada Department of Resources and Development, entitled "Red River Basin Investigation" (R.R.B.I.). Although a few modifications and additions have been made by the Manitoba Water Resources Branch, the methods outlined in the R.R.B.I. report are still being used for flood forecasting in conjunction with the operation of the Red River Floodway.

To facilitate the efficient operation of flood control works and to supply as much advance flood danger warning as possible, a Flood Forecasting Committee was established in 1954. The Committee is composed of technically qualified representatives of all three levels of government who scrutinize and approve all information obtained from contributing agencies in both Canada and the United States and on the basis of these data, prepare forecasts of spring runoff potential for use of the Government of Manitoba. Although the main concern of the Committee is flooding on the Red River, spring peaks are also forecast on the main tributary of the Red River in Manitoba - the Assimboine River. The Committee holds two regular meetings each year - one in February and one in March and as many more meetings as are deemed necessary depending on the severity of flood conditions from year to year. It is the aim of this report to describe the methods used in deriving these flood forecasts.

The drainage basin of the Red and Assiniboine Rivers, together with existing flood control works and dams, is shown on Figure 1.

HYDROMETEOROLOGICAL NETWORKS FOR OPERATION OF THE RED RIVER FLOODWAY

1. Precipitation

Precipitation data in the Canadian portion of the Red River and Assimiboline River Basins are compiled by the Water Resources Branch of the Manitoba Department of Mines and Natural Resources from the network of climatological and meteorological stations maintained by the Meteorological Branch, Canada Department of Transport. Precipitation data from the portion of Red River Basin in the U.S.A. is compiled from the climatological station network maintained by the Environmental Science Service Administration (E.S.S.A.), United States Department of Commerce. The stations in these networks used in connection with operation of the Floodway are shown in Tables I and II.

2. Soil Moisture

Soil moisture throughout the Canadian portion of the Red River
Basin at freeze-up each year is determined by the Manitoba Water Resources
Branch. These surveys began in 1955. The locations of soil moisture survey
stations in the Red River Basin, excluding the Assimiboine River Basin, are
shown in Table III. The Soil Moisture network in the Assimiboine River Basin
is shown in Table IV.

3. Snow Survey

Snow surveys are conducted by the Manitoba Water Resources Branch in mid-February and mid-March throughout Manitoba and portions of Saskatchewan. These surveys began in 1952. The locations of the snow survey stations in the Red River Basin are shown in Table V. Table VI lists the snow survey stations in the Assimboine River Basin.

In addition to the snow surveys undertaken by the Manitoba Water Resources Branch, data are obtained from the snow survey network maintained by

E.S.S.A. in the U.S. portion of the Red River Basin. Stations comprising this network are listed in Table VII.

4. <u>Hydrometric</u>

A hydrometric network is co-operatively maintained in the Canadian portion of the Red River Basin by the Water Survey of Canada and the Manitoba Water Resources Branch.

The hydrometric stations from which up to date data are collected and compiled by the Water Resources Branch in the Canadian portion of the Red River Basin insofar as operation of the Red River Floodway is concerned are shown in Tables VIII and IX.

In the United States portion of the Red River Basin a comprehensive hydrometric network is maintained by the United States Geological Survey. The stations in this network from which data are compiled by the Manitoba Water Resources Branch are shown in Table X.

In addition to the above information, more intensive information on the above-named parameters is obtained from four small watersheds within the Red River Basin and two small watersheds in the Assiniboine River Basin which are used as index areas to provide early indications of the rate and amount of runoff from the winter snow pack. These index areas are described in detail in the following section.

FLOOD FORECASTING PROCEDURES - RED AND ASSINIBOINE RIVERS

A. Preliminary Forecasts (prepared in Late February and Late March)

1. Red River

- a) Evaluation of Forecast Parameters
 - (i) Soll Moisture and Snow Surveys

Soil moisture survey information has not been used quantitatively in the forecast system to date. However, it does provide a qualitative assessment of the moisture conditions of the watershed near the time of freeze-up. Similarly, the results of snow surveys are not being used directly in the models developed for forecasting runoff. However, the information is critically examined and estimates of potential runoff are made using a range of runoff coefficients and these results are compared to the forecasts derived from the runoff-precipitation model. The snow survey results also give an indication of the over-winter depletion of the snow pack, which can be quite substantial under certain meteorological conditions.

(ii) Soil Priming Index

For the Red River Basin, winter streamflow at Emerson measured by the Water Survey of Canada is used as an index of antecedent soil moisture conditions. Natural flows are computed using information on reservoir releases supplied by the United States Army Corps of Engineers at St. Paul Minnesota. Mean monthly natural flows at Emerson are determined for the months of October through January. The sum of these monthly flows is then compared to the long-term mean of natural flows for this period. Expressed as a percent, this constitutes the Soil Priming Index for the Red River Basin above Emerson.

(111) Winter and Spring Precipitation

Monthly winter precipitation for the Red River Basin above Emerson is determined by the Thiessen Polygon Method using the stations listed in

Table I. The period of accumulation is assumed to be from the time of freeze-up to March 31st. Unless the time of freeze-up comes unusually late, the total precipitation for the month of November is included into the estimate of the snowpack. Since the preliminary forecasts are issued prior to March 31st, it is necessary to estimate the snowfall from the time of the forecast until March 31st. This estimate simply consists of the long term mean precipitation for the period in question. In addition, precipitation during the melt period must also be estimated. This estimate is made on the basis of melt period precipitation which has occurred during the period 1915 to date.

(iv) Melt Index

The degree-day method with a base of 32 degrees is used. A mass curve of degree-days is drawn for the index station which is Fargo, North Dakota. Pre-liminary forecasts make use of the average melt index for the period 1915 to date.

b) Preliminary Forecast Procedures

(i) Graphical Method

Forecasts of runoff volume at Emerson are prepared using the graphical model in the R.R.B.I. report. This co-axial relationship is shown on Figure 2. The four parameters required to forecast the runoff are determined by the methods outlined above. Two values of runoff are calculated according to two conditions:

Condition 1 - Normal precipitation and temperatures during melt period. and Condition 2 - (somewhat more severe) - Precipitation and temperatures during melt period = $\frac{1}{2}$ Normal + $\frac{1}{2}$ Maximum on Record.

Applying these forecasts of runoff to a unit hydrograph developed from data presented in the R.R.B.I. report and shown in Table XI, and by adding the estimated base flow of 2000 cfs., a peak flow at Emerson is obtained. The

corresponding peak stage is computed from stage-discharge data provided by the Water Survey of Canada. A peak stage relationship, which has been modified from that in the R.R.B.I. report to take cognizance of rating curve changes since 1950, is used to estimate the peak stage at Winnipeg that would result without flood control works. The peak stage relationship is shown on Figure 3. The effect of flood control works is computed and a forecast is made for the peak stage at Winnipeg.

(ii) Statistical Method

A statistical analysis of 30 high flow years of the Red River at Emerson was carried out by the Water Resources Branch in 1970. The 30 cases were selected from the period of record between 1913 and 1970. The following parameters, used as independent variables in the multi-linear regression analyses, were evaluated for the Red River Basin above Emerson:

- (M.I.) Melt Index
- (W.P.) Winter Precipitation
- (M.P.) Melt Period Precipitation
- (S.I.) Soil Priming Index

Melt indices were determined from mass diagrams of degree-days at Grand Forks, North Dakota; degree-days were calculated on a base of 32 degrees. Precipitation over the basin was found on a monthly basis (or parts of a month when necessary) by calculating the arithmetic mean of the available records. The arithmetic mean was used for simplicity after several test cases revealed little difference between this and the corresponding values obtained by the Thiessen Polygon method. The period of snow accumulation was taken from the time of freeze-up to the break-up. For the analysis of peak flows, precipitation occurring later than two days prior to the date of the peak was excluded from the melt period precipitation. Values for the

Soil Priming Index were calculated from natural flows at Emerson in the same manner as in the graphical method.

The following predictive equations resulted from the analysis:

Standard Error of Estimate = 9455

The estimated peak flow at Emerson is obtained either directly from equation 2 or by applying an appropriate unit hydrograph to the forecast runoff.

The peak stage at Winnipeg is then estimated as described under "Graphical Method".

2. Assimboine River

- a) Evaluation of Forecast Parameters
 - (1) Soil Moisture and Snow Surveys

As in the case of the Red River Basin, the results of these surveys have not been used directly in forecasting up to this time, but provide useful, qualitative information.

(ii) Ground Water Index

An index of antecedent soil moisture conditions is obtained from the precipitation stations listed in Table II. The method used generally follows procedures as outlined in "Report - Conservation and Flood Control - Assimboine River" prepared by the Prairie Farm Rehabilitation Administration (P.F.P.A.) in 1952. Monthly precipitation for the months June - October is determined by the Thiessen Polygon method. The monthly precipitation values are then weighted by the following multiplying factors:

June X 0.2
July X 0.4
August X 0.6
September X 0.8
October X 1.0

The sum of the weighted values is then compared to the same long-term mean value to obtain a percent of normal which constitutes the ground water index for that year.

(11i) Accumulated Precipitation

This parameter is calculated as outlined in the P.F.R.A. report in the following manner:

Accumulated precipitation = Pw + 2Pms + Pmr

where Pw = winter precipitation

Pms = snowfall during the melt period

Pmr = rainfall during the melt period.

Monthly precipitation is determined by the Thiessen Polygon method using the precipitation stations listed in Table II. The period of snow accumulation for Pw is assumed to be November 1st to March 31st. As in the case of the Red River procedures, snowfall from the time of the forecast to March 31st is obtained from long-term means. Values of Pms and Pmr used in preliminary forecasts are their long term mean.

(iv) Melting Index

The following relationships as outlined in the P.F.R.A. report are used:

Molting Index = $Ti + 2Pmr + (Z \times 0.2)$

where Ti = temperature index based on average number of degree-days/day

for 16 index stations during the melt period (base 32 degrees)

Z = number of days before or after April llth that the middle of the melting period occurred.

Preliminary forecasts make use of the long term mean melting index.

- b) Preliminary Forecast Procedures
 - (1) Graphical Model

The graphical relationship developed in the 1952 P.F.R.A. report

is used to derive the most probably runoff coefficient. This relationship is shown on Figure 4. Three parameters are entered into the graphical model and these are calculated as outlined above. The runoff coefficient thus derived is used to compute the runoff based on the snowpack. Estimates of peak flow at Brandon, Portage la Prairie and Headingley are computed by means of basic hydrographs and peak stage relationships. Table XII shows basic hydrographs for various sub-basins within the Assimboine River watershed. Millwood Rivers and Brandon hydrographs are used in conjunction with the curve for Basins 1 to 5 in Figure 4, while Tantallon and Wawanesa are used with the curve for Basins 6 to 10.

(ii) Additional Forecast Procedures

A forecast procedure for the drainage area of the Assimboline River between Brandon and Portage la Prairie was developed by the Water Resources Branch in 1970. Multiple linear regression analyses were carried out on data from 15 flood years during the period 1923-1969. The following four parameters are used as independent variables in the analyses:

(M.I.) Melt Index

(W.P.) Winter Precipitation

(M.P.) Melt Period Precipitation

(A.P.I.) Antecedent Precipitation Index

One of the predictive equations derived is as follows:

Runoff = 0.53920 - 0.14398 (M.I.) + 0.52438 (W.P.)

(inches) + 0.20948 (M.P.) + 0.40816 (A.P.I.)

Multiple Correlation coefficient = 0.97

Standard Error of Estimate = 0.10

For preliminary forecasts, M.I., M.P. and a small part of W.P. are estimated from their long-term mean. The runoff thus calculated is applied

to an appropriate unit hydrograph to yield the forecast hydrograph of flow for the drainage area. Estimated flows of the Assiniboline River at Brandon and the Souris River at Wawanesa are routed by the Muskingum method to Portage la Prairie and added to the forecast hydrograph obtained above to yield the final anticipated flows at Portage la Prairie.

3. Accuracy of Preliminary Forecasts

The graphical model used in preliminary forecasting of runoff volumes for the basin of the Red River above Emerson, shows a correlation of 0.88 between the forecast and actual values. This correlation is based upon a sample of 34 years of data in which the parameters used in the model were calculated from known data. The standard error of estimate is 0.28 inches of runoff while the mean runoff is 0.87 inches.

The correlation between actual peak flows at Emerson and those forecast during March according to Condition 1 is 0.71. This correlation is based upon seventeen spring forecasts issued since 1954. The standard error of estimate is 12,980 c.f.s. and the mean peak is 26,650 c.f.s.

The correlation between actual peak flows on the Assimiboine River at Headingley and the March forecast peak according to Condition 1 is 0.91. The standard error of estimate is 2,330 c.f.s. and the mean peak for the seventeen cases is 10,820 c.f.s.

A summary of forecast and actual peak flows for the Red River at James Avenue in Winnipeg is shown on Figure 5. The histograms labelled "NORMAL" and "EXTREME" refer to Conditions number 1 and 2 respectively, as explained under Preliminary Forecast Procedures of the Red River.

The accuracies of the statistical forecast methods are indicated above, together with their predictive equations. It should be emphasized that the statistical method has not been used thus far in issuing preliminary

forecasts on the Red River, rather the graphical method is used.

Errors in preliminary forecasts have no effect on the operation of the Red River Floodway since the actual operation of flood control works is based upon operational forecasts which are described in the following sections.

B. Operational Forecasts (When Runoff Has Commenced)

1. Red River

a) U.S. Data

E.S.S.A. forecasts for Emerson are generally used although modificiations may be made after interpretation of hydrometric data from stations shown in Table X. During major floods, the Water Resources Branch has an employee stationed at Fargo to provide liaison between United States agencies and the Manitoba Water Resources Branch and to ensure that pertinent up-to-date information is exchanged.

b) Index Areas

A very useful tool in runoff forecasting from snow melt is the index area. This is particularly true in large basins having prolonged runoff characteristics such as the Red and Assimboine River Basins. Runoff from snow melt in small tributary drainage basins is usually over well before the time when runoff is well advanced over the whole basin. By measuring the available snowpack along with the precipitation during the runoff period and comparing the available moisture to the measured runoff, the percentage runoff is determined. The runoff coefficient thus obtained can be applied over large areas and an appraisal can be made of the expected runoff and peak flows.

To provide an estimate of runoff coefficients in the Red River Basın, four index areas are used: the south branch of the Buffalo River

at Sabin, Minnesota; the Tongue River at Akra, North Dakota; Dead Horse Creek at Morden, Manitoba; and Rosengart Coulee near Sarto, Manitoba. Detailed snow surveys are made on these areas just prior to runoff. These are followed by an intensive hydrometric program after runoff has commenced. Estimates of the runoff coefficient are made and corrected as runoff progresses. These runoff coefficients are applied to larger areas and estimates of peak flows at various points along the Red River are made. The Tongue River and Rosengart Coulee have not proven as satisfactory as the South Branch of the Buffalo River and Dead Horse Creek and an attempt will be made to establish more satisfactory index areas in these vicinities.

c) Hydrometric Data

Hydrometric data are obtained at the stations shown in Table VIII.

These data are used in updating and modifying forecast magnitude and date
of peak flows on the Red River.

d) Canadian Tributary Runoff

An estimate of the tributary runoff hydrographs for those major streams downstream from Emerson is made using snow survey data and various runoff coefficients. Unit hydrographs shown in the R.R.B.I. report are used for the western tributaries, whereas unit hydrographs as revised by the Manitoba Water Resources Branch are used for the eastern tributaries. As the runoff progresses and data as to the runoff situation becomes available, forecast tributary runoff is adjusted.

e) River Routing

Routings are undertaken on a digital computer using the Muskingum method. Emerson flows, tributary flows and estimated ungauged flows are routed from Emerson to Ste. Agathe and from Ste. Agathe to Winnipeg. The flows thus derived are added to the expected natural flows on the Assinibolne

River at Headingley and to local gauged and ungauged flows entering the system near Winnipeg to derive the total flow and associated stage at Winnipeg which would have resulted without the use of flood control works. The flow to be diverted through the Red River Floodway is then determined in a manner which ensures that water levels above the floodway inlet will not exceed levels which would have occurred under natural conditions. The remaining flow through the City is added to the anticipated flow on the Assinibolne River after the effects of the Shellmouth Reservoir and the Portage Diversion have been considered. This yields the anticipated flow and associated stage at Winnipeg with flood control works in use.

2. Assiniboane Raver

Hydrometric gauging stations for the Assimboline River are listed in Table IX. The preliminary forecast issued in March is updated using hydrometric data as it arrives. Oak Creek near Stockton and Conjuring Creek near Russell are closely observed as index areas as a check on melt rates and runoff coefficients. Hydrometric data are assembled each day from the stations listed in Table IX, and runoff rates are modified daily on the basis of these data.

Flashy runoff frequently results from the drainage area of the Assiniboine River between Brandon and Portage la Prairie. The forecast procedures for this area, described under "Preliminary Forecasts" are applied to facilitate operation of the Portage Diversion.

A river routing procedure to be used in the operational forecasting of the Assiniboine River flood flows is being developed at the present time.

3. Accuracy of Forecasts

Since operational forecasts are revised from day to day as necessary, it is difficult to describe the accuracy of these forecasts. However, it would be correct to say that generally the earlier operational forecasts verify better than the preliminary forecasts and that the accuracy of the operational forecasts increases with time as more information becomes available. The operation of the Red River Floodway as well as of other flood control works is based on the flood situation at the time and on the latest available forecasts.

TABLE I

Precipitation Stations - Red River Basin

U.S. Portion

Ada Adams Amenia Angus Argyle Campbell Colgate Cooperstown Crookston Detroit Lakes Elbow Lake Enderlin Fargo Fergus Falls Fosston Forman Gonvick Goodridge Grafton Grand Forks Hallock Hankinson Harvey Hawley Herman High Landing Hillsboro

Langdon
Larimore
Lisbon
Litchville
Mahnomen
Mayville
McHenry
McLeod
McVille
Oklee
Ottertall
Park River
Pelican Rapids
Pembina

Pembina Petersburg Red Lake Falls Red Lake Ind. Ag. Roseau

Roseau Sharon Sheyenne

Thief Lake Refuge Thief River Falls

Trail
Valley City
Wahpeton
Wheaton

Canada Portion

Altona
Boissevaln
Emerson
Graysville
Morden (Exp. Farm)

Morris (Exp. St.) Ste. Genevieve Sprague

Sprague Winnipeg

TABLE II

Precipitation Stations - Assimiboine River Basim

Baldur

Birtle

Bottineau

Brandon

Broadview

Carberry

Carlyle

Caron

Ceylon

Chaplin

Crosby

Cypress River

Davidson

Dauphin

Deerwood

Dilke

Estevan

Francis

Foam Lake

Grenfell

Hubbard

Indian Head

Kamsack

Lumsden

Melita

Midale

Minnedosa

Minor

Mohall

Moose Jaw

Ninette

Pilger

Portage la Prairie

Regina

Rivers

Rugby

Russell

Semans

Souris

St. Alphonse

Strasbourg

Towner

Treherne

Tugaske

Virden

Waskada

Whitewood

Yellowgrass

Yorkton

TABLE III

Soil Moisture Stations - Red River Basin in Manitoba.

Station No.	Station Location
R-I-1	St. Norbert
R - I - 2	Fannystelle
R - I - 3	Rathwell
R - I - 4	Killarney
R - I - 5	Turtle Mountain
R - I - 6	Morden
R - I - 7	Lowe Farm
R - I - 8	Letellier
R - I - 9	La Riviere
,	
R - II - 1	Ste. Anne
R - II - 2	Steinbach
R - II - 3	Dominion City
R - II - 4	Stuart burn

TABLE IV

Soil Moisture Stations

Assimiboine River Basim in Mamitoba and Saskatchewan

Station No.	Station Location
A - I - 1	Millwood
A - I - 2	Runnymede
A - I - 3	Yorkton
A - I - 4	Canora
A - I - 5	Theodore
A - II - 1	Broadview
A - II - 2	Lipton
A - II - 3	Regina
A - III - 1	Melita
A - III - 2	Carlyle
A - III - 3	Benson
A - III - 4	Estevan
A - III - 5	Weyburn
A - III - 6	Radville
A - IV - 1	Brandon
A - IV - 2	Shoal Lake
A - IV - 3	Virden
A - IV - 4	Moosomin
A - V - 1	Minnedosa
A - V - 2	Wasagaming
A - VI - 1	Portage la Prairie
A - VI - 2	Cypress River

TABLE V

Snow Survey Stations - Red River Basin in Manitoba

Station No.	Station Location
C - 1	Fannystelle
C - 2	Rathwell
C - 12	Turtle Mountain
C - 13	Killarney
C - 14	La Riviere
C - 15	La Riviere
C - 16	Morden
C - 17	Carman
C - 18	St. Norbert
D - 12	Gretna
D - 13	Morris
D - 1	Beausejour
D - 7	Ste. Anne
D - 8	Sandilands F.R.
D - 9	${ t Vassar}$
D - 10	Sluartburn
D - 11	Dominion City
D - 14	St. Pierre

TABLE VI

Snow Survey Stations

Assimiboine River Basin in Saskatchewan and Mamitoba

Station No. 1	Station Location
A - 15 A - 17 A - 18 A - 19 B - 6 B - 7 B - 8 B - 9 B - 10 B - 11 B - 12	Watson Wynyard Sheho Yorkton Russell Roblin Madge Lake S. Madge Lake N. Kamsack Canora Tall Pines, Porcupine F.R.
A - 9 A - 10 A - 11 A - 12 A - 13 A - 14 A - 20	Broadview Indian Head Regina Moose Jaw Penzance Watrous Churchbridge
A - 6 A - 7 A - 8 B - 4 B - 5	Kenton Virden Moosomin Shoal Lake Birtle
B - 3 B - 26 B - 27 A - 5	Minnedosa Rıding Mountaın Wasagəming Rivers
C - 4 C - 5 C - 6 C - 7 C - 8 C - 9 C - 10 C - 11	Wawanesa Souris Sinclair Carlyle Hume Estevan Oxbow Melita
A - 1 A - 4 C - 3	Portage la Prairie Brandon Cypress River

TABLE VII

Snow Survey Stations - Red River Basin in the United States

Abercrombie

Crookston

Fargo

Grand Forks

High Landing

Pembina

Wahpeton

Bald Hill

White Rock Dam

Park River

Ada

Argyle

Cavaller

Amenia

Agassız Refuge

Campbell

Chaffey

Colgate

Detroit Lakes

Halstad

Drayton

Fosston

Foreman

Hallock

Larimore

Lisbon

Mayville

Mahnomen

McLeod

Thief River Falls

Walhalla

Valley City

TABLE VIII HYDROMETRIC STATIONS - RED RIVER BASIN IN CANADA

Red River

	Station No.	<u>Latitude</u>	Longitude
James Ave. Pumping Station South Perimeter Bridge Below Floodway Inlet Above Floodway Inlet St. Adolphe		49° 53° 56° 49° 47° 10° 49° 45° 20° 49° 45° 10° 49° 40° 27°	97° 07' 47" 97° 08' 13" 97° 08' 10" 97° 08' 00" 97° 06' 55"
Ste. Agathe	0500012	490 331 4011	970 101 52"
Morris St. Jean	0500006	49° 21° 30" 49° 16° 07"	97° 21' 00" 97° 20' 56"
Letellier	0500010	49° 07° 54"	97° 20' 36" 97° 15' 16"
Emerson	0500001	490 001 3011	970 121 40"
Aubigny		49° 27° 34"	97° 16° 15"
Red River Tributaries			
Roseau River @ Langside Bridge	0500003	49° 11 ' 53"	97° 03° 15"
Roseau River @ Gardenton	050D004	49° 05° 16"	96° 41° 15"
Roseau River @ International			,
Building	050D007	49° 00° 10°°	96° 291 40"
Scine River Diversion @ P.T.H. #59	0.00000	100 120 100	0/0 504 505
Scine River @ Prairie Grove	05011008 050H006	49° 41° 40" 49° 46° 15"	96° 591 1911 96° 561 1011
Seine River @ P.T.H. #59	0,00000	490 451 5311	97° 01° 42"
Prairie Grove Drain @		47 72), OT 4"
P.T.H. #59		49° 41' 40"	96° 59° 19"
Main Drain 4A @ Dominion City	050D028	49° 08' 01"	970 081 4211
La Salle River E 33-8-2E La Salle River Q Sanford	0506001	49° 41 ' 38'' 49° 40 ' 52''	97° 15° 48° 97° 25° 48°
La Salle River @ Elie	0300001	49° 54° 48°	97° 25° 48" 97° 45° 27"
Morris River @ Morris	050F001	490 211 5011	970 221 7511
Plum River @ St. Jean		49° 16° 04"	97° 211 1211
Tourond Creek @ P.T.H. #59		49° 31° 50°	96° 581 50"
Rat River @ Otterbourne	050E001	490 271 4211	970 001 26"
Dead Horse Creek @ Morden Rosengart Drain NE 32-5-6E	0500015	49° 11' 34" 49° 26' 48"	98° 06' 40" 96° 44' 01"
Rosengart Drain E 26-5-6E		49° 24† 37#	96° 441 01" 96° 391 40"
Rosengart Drain E of P.T.H. 12		49° 231 3811	960 411 02"
Rosengart Drain S 35-5-6E		49° 241 5411	96° 401 48"

TABLE IX

HYDROMETRIC STATIONS - ASSINIBOTNE RIVER BASIN

Assiniboine River

	Station No.	<u>Latitude</u>	Longitude
Kamsack Shellmouth Dam Roblin	05MD004	51° 33† 38" 50° 57† 58" 51° 13† 38" 50° 41† 25"	101° 54° 40° 101° 25° 21° 101° 38° 39° 101° 26° 09°
Mıllwood Russell St. Lazare Vırden Grıswold	05ME001	50° 48° 35" 50° 26° 38" 49° 50° 31" 49° 50° 33"	101° 26° 10° 101° 20° 10° 10° 48° 01° 10° 27° 20°
Brandon	05MH001	490 511 02"	99 ⁰ 561 1211
Holland	05MH005	490 411 4011	98 ⁰ 53† 2011
Portage la Prairie	05MJ003	490 561 0911	98 ⁰ 16† 48††
Bare St. Paul	0747003	50° 02° 37"	97° 521 11"
Headingly	05MJ001	49° 52° 09° 49° 51° 38°	97° 24° 10° 98° 26° 43°
Hood Bridge		49° 51° 38° 49° 56° 06°	98° 16° 56° 98°
Southport Miniota	0511E006	1010 021 08"	500 061 3911
Rossendale	05MJ005	49° 45° 32"	98° 381 32"
Assiniboine Fiver Tributaries		4, 4, 3,	, , , , , , , , ,
Au'Appelle River © Tantallon Minnedosa River © Minnedosa Minnedosa River @ Rivers	05MJ003 05MF001 05NF020	50° 31° 58° 50° 21° 28° 50° 01° 37°	101° 50† 13" 99° 54† 00" 100° 01† 58"
Souris River @ Wawanesa Sturgeon Creek near Grace Hospital	05NG001 05MJ004	49° 36° 05° 49° 52° 35°	99° 40° 55° 99° 02° 00°

TABLE X

Hydrometric Stations - Red River Basin in the United States

Marsh River Marsh River Wild Rice River Wild Rice River Wild Rice River Sandhill River Clearwater River Clearwater River Little Pembina R. Sheyenne River Buffalo River Buffalo River Buffalo River Buffalo River Cart Creek Cart Creek Cart Creek Forest River Forest River Forest River Park River Park River Park River Park River (N.Br.) Park River (S.Br.)	@ Ada @ Shelley @ Ada @ Abercromble @ Twn Valley @ Climax @ Red Lake Falls @ Plummer @ Oklee near Walhalla @ Kindred @ Cooperstown @ Lisbon @ Valley City @ West Fargo @ Sprague @ Dillworth @ Hawley @ Sabin @ Downe @ Hendrum @ Mountain @ Crystal @ Whitman @ Fordville @ Minto @ Union @ Grafton @ Garden @ below Homme Dam	S. Branch Two River Red River Roseau River	vers @ Lake Bronson vers @ Hallock @ Grand Forks @ Fargo @ Oslo @ Drayton @ Wahpeton @ Halstad @ Pembina @ Roseau Lake @ Roseau @ Badger @ Caribou @ Ross
	@ Grafton		
Park River (N.Br.)	@ Garden	Roseau River	@ Carıbou
Park River (S.Br.)	@ below Homme Dam	Roseau River	@ Ross
Park River	@ Adams	Roseau River	@ Malung
Maple River	@ Hope	Roseau River	below South Forks
Maple River	© Mapleton		

Unit Hydrographs at Emerson, Paritoba

(Based on Plates 19 and 20 'nparaly C - R.F.B.I. 1952)

Day 12-Hour 21-Hour 36-Hour 48-Hour 60-Hour 72-Hour 81-Hour 60-Hour 72-Hour 81-Hour 60-Hour 73-Hour 81-Hour 60-Hour 74-Hour 81-Hour 60-Hour 74-Hour 81-Hour 60-Hour 74-Hour 81-Hour 60-Hour 74-Hour 81-Hour 75-Hour 81-Hour 75-Hour 81-Hour 75-Hour 81-Hour 75-Hour 81-Hour 75-Hour 81-Hour 75-Hour			Time	-Base of Uni	t Hydrograph	l		
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1 500 350 250 190 150 120 110 390 30 390 3 1,200 1,200 110 830 690 550 160 390 30 2,450 2,030 1,730 1,360 2,670 2,360 5 8,300 7,500 6,700 6,030 5,350 3,040 2,670 2,360 6 12,700 11,600 10,500 9,550 8,660 7,880 7,160 7 18,200 16,800 15,530 14,280 13,000 12,020 11,030 8 23,300 22,250 20,500 19,600 18,220 16,930 11,570 9 29,400 28,100 26,500 25,180 23,780 22,150 22,470 10 32,600 32,050 31,160 50,000 35,500 31,400 34,100 33,600 35,500 35,600 35,500 35,600 35,500 35,600 35,500 35,500 35,480 35,200 31,420 30,260 11,330 35,300 35,600 35,500 35,500 35,500 35,480 35,200 32,850 31,400 32,800 32		c.f.s.	c f.s.	c.f c	c.f.s	c.fr.	c.f.s	c.fs.
1 500 350 250 190 150 120 110 390 30 390 3 1,200 1,200 110 830 690 550 160 390 30 2,450 2,030 1,730 1,360 2,670 2,360 5 8,300 7,500 6,700 6,030 5,350 3,040 2,670 2,360 6 12,700 11,600 10,500 9,550 8,660 7,880 7,160 7 18,200 16,800 15,530 14,280 13,000 12,020 11,030 8 23,300 22,250 20,500 19,600 18,220 16,930 11,570 9 29,400 28,100 26,500 25,180 23,780 22,150 22,470 10 32,600 32,050 31,160 50,000 35,500 31,400 34,100 33,600 35,500 35,600 35,500 35,600 35,500 35,600 35,500 35,500 35,480 35,200 31,420 30,260 11,330 35,300 35,600 35,500 35,500 35,500 35,480 35,200 32,850 31,400 32,800 32	•	•	•	•	•	•	•	_
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7	5		7,500	6,700		5,380	4,830	4,310
8		12,700	11,600			8,660	7,880	
9		18,200	16,800	15,530		13,080	12,020	
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15 32,400 32,800 33,300 33,730 34,040 34,350 34,630 16 29,900 30,500 31,100 31,680 32,200 32,650 33,030 18 23,900 27,550 25,300 26,600 27,520 22,250 23,200 24,630 25,590 28,210 19 21,200 21,850 22,500 23,200 23,920 24,630 25,590 22,500 23,920 24,630 25,590 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 22,130 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 22,670 21,340 21,970 21,940	13		35,600	35,800	35 , 750	35,480		31.,830
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17 24 600 27 600 26 700 26 700 26 600 27,520 26 40 18 23,900 21,550 25,300 26,300 26,600 27,520 28,210 19 21,200 21,850 22,500 23,200 23,340 21,980 22,670 20 19,100 19,550 20,100 20,700 21,340 21,980 22,670 21 17,400 17,700 18,200 18,630 19,140 19,700 20,300 22 15,300 15,800 16,300 16,750 17,220 17,680 16,190 23 13,700 14,050 14,500 14,930 15,420 15,850 16,310 24 12,600 12,600 12,200 12,500 12,820 14,670 25 11,300 11,600 12,000 12,200 12,500 12,820 13,170 26 10,300 10,550 10,800 11,080 11,380 11,650 11,940	16	29,900	30,500	31,100	31,680		32,650	33,030
19 21,200 21,850 22,500 23,200 23,920 24,630 25,390 20 19,100 19,550 20,100 20,700 21,340 21,970 22,670 21 17,400 17,700 18,200 18,630 19,140 19,700 20,300 22 15,300 15,800 16,300 16,750 17,220 17,680 18,190 23 13,700 14,050 14,930 15,420 15,850 16,310 24 12,600 12,800 13,300 13,330 13,800 14,220 14,670 25 11,300 11,600 12,000 12,500 12,820 13,170 26 10,300 10,550 10,800 11,080 11,380 11,650 11,940 27 9,500 9,700 9,900 10,130 10,360 10,620 10,900 28 8,800 9,000 9,200 9,350 9,540 9,750 9,830 29	77	3K BUU					ີລບົວຜບ -	
19 21,200 21,850 22,500 23,200 23,920 24,630 25,390 20 19,100 19,550 20,100 20,700 21,340 21,970 22,670 21 17,400 17,700 18,200 18,630 19,140 19,700 20,300 22 15,300 15,800 16,300 16,750 17,220 17,680 18,190 23 13,700 14,050 14,930 15,420 15,850 16,310 24 12,600 12,800 13,300 13,330 13,800 14,220 14,670 25 11,300 11,600 12,000 12,500 12,820 13,170 26 10,300 10,550 10,800 11,080 11,380 11,650 11,940 27 9,500 9,700 9,900 10,130 10,360 10,620 10,900 28 8,800 9,000 9,200 9,350 9,540 9,750 9,830 29	18	23,900	21,550	25,300	26,030	26, 800	27,527	28, 210
20 19,100 19,550 20,100 20,700 21,340 21,980 22,670 21 17,400 17,700 18,200 18,630 19,140 19,700 20,300 22 15,300 15,800 16,300 16,750 17,220 17,680 18,190 23 13,700 14,050 14,500 14,930 15,420 15,850 16,310 24 12,600 12,800 13,000 13,330 13,800 14,220 14,670 -25 11,300 11,600 12,000 12,200 12,500 12,820 13,170 26 10,300 10,550 10,800 11,080 11,380 11,650 11,940 27 9,500 9,700 9,900 10,130 10,360 10,620 10,900 28 8,800 9,000 9,200 9,350 9,540 9,750 9,830 29 8,200 8,300 8,500 8,650 8,820 9,000 9,190 30 7,500 7,600 7,800 7,980 8,140 <t< th=""><td>19</td><td>21,200</td><td>21,850</td><td>22,500</td><td>23, 200</td><td>23,920</td><td>24,630</td><td>25,290</td></t<>	19	21,200	21,850	22,500	23, 200	23,920	24,630	25,290
21 17,400 17,700 18,200 18,630 19,140 19,700 20,300 22 15,300 15,800 16,300 16,750 17,220 17,680 18,190 23 13,700 14,050 14,500 14,930 15,420 15,850 16,310 24 12,600 12,800 13,000 13,330 13,800 14,220 14,670 25 11,300 11,600 12,000 12,200 12,500 12,820 13,170 26 10,300 10,550 10,800 11,080 11,380 11,650 11,940 27 9,500 9,700 9,900 10,130 10,360 10,620 10,900 28 8,800 9,000 9,200 9,350 9,750 9,750 9,830 29 8,200 8,300 8,500 8,500 8,820 9,000 9,190 30 7,500 7,650 7,800 7,980 8,140 8,320 8,490 31 7,100 7,200 7,300 7,430 7,580 7,720<	20	19,100	19,550		20,700		21,980	22,670
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26 10,300 10,550 10,800 11,080 11,380 11,650 11,940 27 9,500 9,700 9,900 10,130 10,360 10,620 10,900 28 8,800 9,000 9,200 9,350 9,540 9,750 9,830 29 8,200 8,300 8,500 8,650 8,820 9,000 9,190 30 7,500 7,650 7,800 7,980 8,140 8,320 6,490 31 7,100 7,200 7,300 7,430 7,580 7,720 7,870 32 6,600 6,700 6,800 6,950 7,060 7,180 7,330 33 6,200 6,250 6,400 6,460 6,720 6,830 34 5,700 5,800 5,900 6,030 6,140 6,250 6,370 35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,100 5,180 5,260 3	-25						12,820	13,170
27 9,500 9,700 9,900 10,130 10,360 10,620 10,900 28 8,800 9,000 9,200 9,350 9,540 9,750 9,830 29 8,200 8,300 8,500 8,650 8,820 9,000 9,190 30 7,500 7,650 7,800 7,980 8,140 8,320 6,490 31 7,100 7,200 7,300 7,430 7,580 7,720 7,870 32 6,600 6,700 6,800 6,950 7,060 7,180 7,330 33 6,200 6,250 6,400 6,400 6,600 6,720 6,830 34 5,700 5,800 5,900 6,030 6,140 6,250 6,370 35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,120 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 <t< th=""><th></th><th></th><th></th><th>10.800</th><th></th><th></th><th>11,650</th><th></th></t<>				10.800			11,650	
28 8,800 9,000 9,200 9,350 9,540 9,750 9,830 29 8,200 8,300 8,500 8,650 8,820 9,000 9,190 30 7,500 7,650 7,800 7,980 8,140 8,320 6,490 31 7,100 7,200 7,300 7,430 7,580 7,720 7,870 32 6,600 6,700 6,800 6,950 7,060 7,180 7,330 33 6,200 6,250 6,400 6,400 6,600 6,720 6,830 34 5,700 5,800 5,900 6,030 6,140 6,250 6,370 35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,120 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,670 4,730 4,800 4,830 4,960 39						10.360	10,620	
29 8,200 8,300 8,500 8,650 8,820 9,600 9,190 30 7,500 7,650 7,800 7,980 8,140 8,320 6,490 31 7,100 7,200 7,300 7,430 7,580 7,720 7,870 32 6,600 6,700 6,800 6,950 7,060 7,180 7,330 33 6,200 6,250 6,400 6,480 6,600 6,720 6,830 34 5,700 5,800 5,900 6,030 6,140 6,250 6,370 35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,420 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,100 4,570 4,340 41		8,800	9,000	9,200		9,540	9,750	9,830
30 7,500 7,650 7,800 7,980 8,140 8,320 6,490 31 7,100 7,200 7,300 7,430 7,580 7,720 7,870 32 6,600 6,700 6,800 6,950 7,060 7,180 7,330 33 6,200 6,250 6,400 6,480 6,600 6,720 6,830 34 5,700 5,800 5,900 6,030 6,140 6,250 6,370 35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,120 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,430 4,500 4,570 4,340 40 3,900 3,750 3,800 3,850 3,920 3,980 4,060			8, 300		8,650			
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32 6,600 6,700 6,800 6,950 7,060 7,180 7,330 33 6,200 6,250 6,400 6,480 6,600 6,720 6,830 34 5,700 5,800 5,900 6,030 6,140 6,250 6,370 35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,420 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,430 4,500 4,570 4,640 40 3,900 3,950 4,030 4,160 4,180 4,270 4,340 41 3,700 3,500 3,500 3,850 3,920 3,980 4,060 42 3,400 3,500 3,500 3,380 3,440 3,500 3,560	31			7.300		7.580		7,870
33 6,200 6,250 6,400 6,460 6,600 6,720 6,830 34 5,700 5,800 5,900 6,030 6,140 6,250 6,370 35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,420 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,430 4,500 4,570 4,640 40 3,900 3,950 4,030 4,160 4,180 4,270 4,340 41 3,700 3,750 3,800 3,850 3,920 3,980 4,060 42 3,400 3,500 3,500 3,380 3,440 3,500 3,560 43 3,200 3,050 3,100 3,150 3,200 3,270 3,330	32		6, 700	6.800		7.060	7,180	7.330
34 5,700 5,800 5,900 6,030 6,140 6,250 6,370 35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,420 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,430 4,500 4,570 4,640 40 3,900 3,950 4,030 4,100 4,180 4,270 4,340 41 3,700 3,750 3,800 3,850 3,920 3,980 4,060 42 3,400 3,500 3,570 3,630 3,680 3,730 3,800 43 3,200 3,250 3,300 3,380 3,440 3,500 3,300 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330			6.250			6,600	6.720	6.830
35 5,400 5,500 5,600 5,650 5,760 5,850 5,910 36 5,100 5,200 5,270 5,300 5,420 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,430 4,500 4,570 4,640 40 3,900 3,950 4,030 4,100 4,180 4,270 4,340 41 3,700 3,750 3,800 3,850 3,920 3,980 4,060 42 3,400 3,500 3,570 3,630 3,680 3,730 3,800 43 3,200 3,250 3,300 3,380 3,440 3,500 3,560 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330			5,800	5, 900		6.140		
36 5,100 5,200 5,270 5,300 5,420 5,500 5,600 37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,430 4,500 4,570 4,640 40 3,900 3,950 4,030 4,100 4,180 4,270 4,340 41 3,700 3,750 3,800 3,850 3,920 3,980 4,060 42 3,400 3,500 3,570 3,630 3,680 3,730 3,800 43 3,200 3,250 3,300 3,380 3,440 3,500 3,560 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330			5, 500	5,600		5.760	5,850	5,910
37 4,800 4,850 4,930 5,030 5,100 5,180 5,260 38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,430 4,500 4,570 4,640 40 3,900 3,950 4,030 4,100 4,180 4,270 4,340 41 3,700 3,750 3,800 3,850 3,920 3,980 4,060 42 3,400 3,500 3,570 3,630 3,680 3,730 3,800 43 3,200 3,250 3,300 3,380 3,440 3,500 3,560 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330		5.100	5,200	5,270	5,300	5.420	5,500	5,600
38 4,500 4,600 4,670 4,730 4,800 4,830 4,960 39 4,200 4,250 4,330 4,430 4,500 4,570 4,640 40 3,900 3,950 4,030 4,100 4,180 4,270 4,340 41 3,700 3,750 3,800 3,850 3,920 3,980 4,060 42 3,400 3,500 3,570 3,630 3,680 3,730 3,800 43 3,200 3,250 3,300 3,380 3,440 3,500 3,560 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330	37				5 030	5.100	5.180	5, 260
39 4,200 4,250 h,330 4,430 h,500 4,570 L,640 40 3,900 3,950 4,030 4,100 4,180 4,270 4,340 41 3,700 3,750 3,800 3,850 3,920 3,980 4,060 42 3,400 3,500 3,570 3,630 3,680 3,730 3,800 43 3,200 3,250 3,300 3,380 3,440 3,500 3,560 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330			7, 600		1, 730	J. 800	4.830	4, 960
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41 3,700 3,750 3,800 3,850 3,920 3,980 4,060 42 3,400 3,500 3,570 3,630 3,680 3,730 3,800 43 3,200 3,250 3,300 3,380 3,440 3,500 3,560 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330						4.180		
42 3,400 3,500 3,570 3,630 3,680 3,730 3,800 43 3,200 3,250 3,300 3,380 3,440 3,500 3,560 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330					3, 850	3,920	3,980	4.060
43 3,200 3,250 3,300 3,380 3,440 3,500 3,560 44 3,000 3,050 3,100 3,150 3,200 3,270 3,330			3,500			3,680		3,800
44, 3,000 3,050 3,100 3,150 3,200 3,270 3,330				3,300		3.440	3,500	3,560
75 2 800 2 850 2 900 2 950 3 000 3 050 3 100							3,270	3, 330
	45	2,800	2,850	2,900	2,950	3,000	3,050	3,100

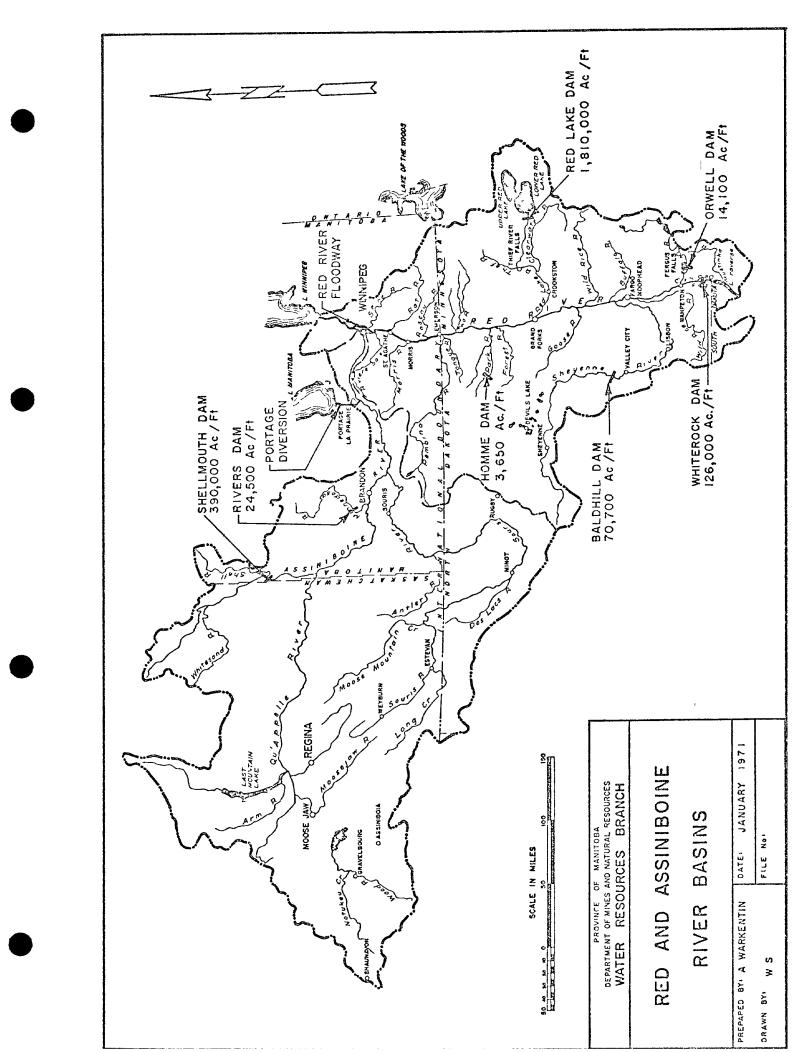
TABLE X11

Basic Hydrographs for Sub-Basins of the Assimboine River

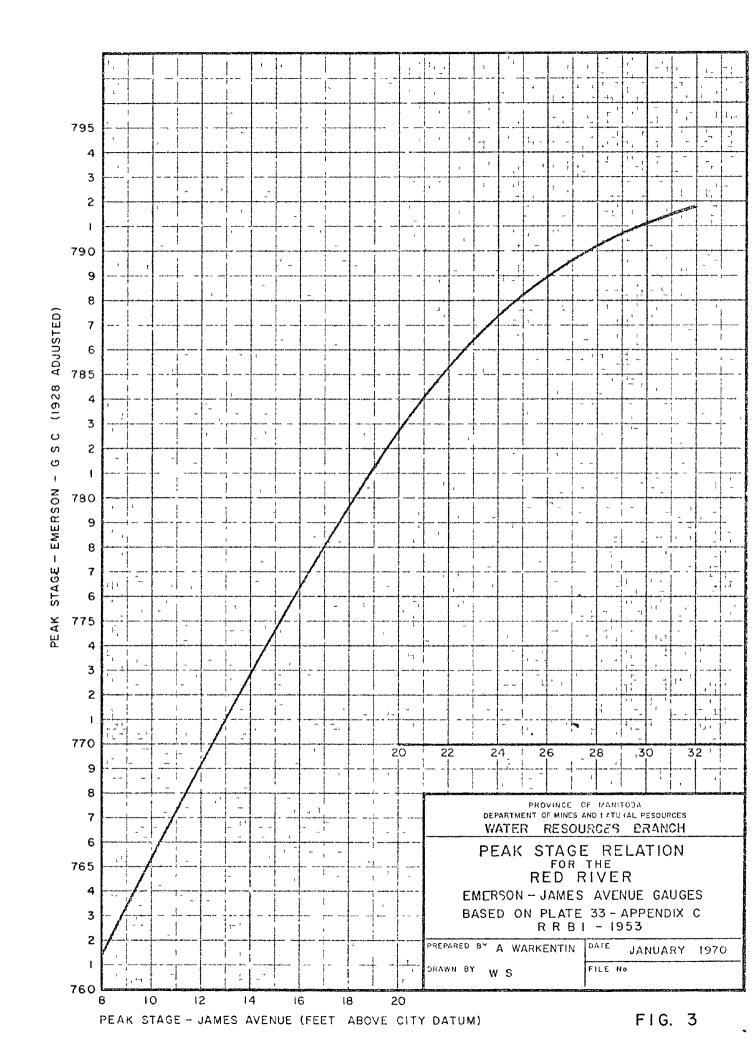
(Based on 1952 P.F.R.A. Report)

Runoff Equivalent in C.F.S per Square Hile

Day	Millwood	Brandon	Rivers	Tantallon	Wawanesa
0	0.00	0.00	0.00	0.00	0.00
ì	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00
3	0.00	0.00	0.00	0.00	0.00
3 4 5 6	0.00	0.10	0.00	0.00	0.00
5	0.00	0.16	0.00	0 00	0.00
6	0.00	0.24	0.00	0.00	0.00
7 8	0.03	0.32	0.00	0.00	0.00
8	0.06	0.42	0.01,	0.00	0.00
9	0.08	0.54	0.08	0.00	0.01
10	0.12	0.70	0.13	0.00	0.02
11	0.15	0.92	0.18	0.00	0.03
12	0.20	1.38	0.24	0 00	0 05
13	0.24	1.80	0.30	0 00 0.03	0.06
14	0.30	2.18	0.38		0.08
15 16	0.37	2.51 2.34	0.44	0.06 0.10	0.10 0.12
17	0.45 0.60	2.36 2.18	0.54 0.61	0.13	0.16
18	0.78	1.96	0.70	0.18	0.20
19	1.04	1.70	0.82	0.24	0.24
20	1.30	1.34	1.00	0.26	0.30
21	1.54	1.04	1.50	0.29	0.37
22	1.72	0.90	1.80	0.31	0.1.4
23	1.64	0.77	1.74	0.34	0.52
24	1.55	0.66	1.68	0.37	0.58
25	1.35	0.59	1.60	0.39	0.59
26	1.19	0.51	1.50	0.1.2	0.60
27	1.08	0.45	1.38	0.1.1.	0 90
28	1.00	0.39	1.22	0.46	0.60
29	0.92	0.33	1.10	0.47	0.59
30	0.86	0.29	1.00	0.48	0.58
31	0.81	0.23	0.89	0.48	0.56
32	0.76	0.17	0.79	0.48	0.55
33	0.72	0.10	0.70	0.48	0.54
34	0.68	0.00	0.63	0.47	0.52
31 32 33 34 35 36 37 38	0.63 0.58		0.57 0.51	0,47 0.47	0.51 0.50
20 27	0.54		0.45	0.46	0.49
36 36	0.49		0.40	0.46	0.48
39	0.45		0.34	0.45	0.47
40	0.40		0.30	0.45	0.46
41	0.36		0.26	0.44	0.45
42	0.32		0.22	0.44	0.44
43	0.27		0.19	0.43	0.43
44	0.23		0.16	0.42	0.1,2
45	0.10		0.13	0.41	0.42
46	0.15		0.11	0.41	0.41
47	0.12		0.09	0.41	0.41
48	0.09		0.07	0.40	0.40
49	0.06		0.05	0.39	0.40
50	0.04		0.03	0.38	0.39



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7		- -					RCES ICH	NOIL	o XIQ	18Y 1971	
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- -				AREA)			PROVINCE OF MANITOBA DEPARTMENT OF NINES AND NATURAL PESOURCES WATER RESOURCES BRANCH	RUNOFF FOR THE	> 5	DATE FILE	
PITATION	,		= 1	INAGE -			PROVINCE NT OF ATE		RED F	WARKENTIN	
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2				(%) OF NORMAL)				The same of the sa	BB III		
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GROUND WATER INDEX		2											02										
01 - 02 SRO	, ,	NOT	TATA9	1038	PP - 5	TED	11/	15-3-11/4		-		-	-	,	· ·								

